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## SPECIFICATION

### CERAMIC FILTER FOR EXHAUST GAS EMISSION CONTROL

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#### RELATED APPLICATION

This application claims priority from Japanese Patent Application No. 2002-72847 filed on March 15, 2002.

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#### TECHNICAL FIELD

The present invention relates to ceramic filters for exhaust gas emission control, and more particularly, to a ceramic filter assembly in which a plurality of filters made of a ceramic sintered material are integrated, a canning body, and a columnar honeycomb filter that may be used when manufacturing the same.

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#### PRIOR ART

The number of automobiles is dramatically increasing, and in proportion thereto, the amount of exhaust gas exhausted from internal combustion engines of automobile is also rapidly increasing. Various substances contained in the exhaust gas, especially from diesel engines cause pollution, and thus presently, are seriously affecting the world environment. Reports have been recently made on study results that fine particles (diesel particulate) in the exhaust gas may sometimes cause allergic symptoms or reduce sperm counts. A measure for eliminating the fine particles in the exhaust gas is thus an urgent problem that must be coped with for the sake of mankind.

Accordingly, a variety of exhaust gas purifying devices have been proposed in the prior art. A typical exhaust gas purifying device has a configuration in which a casing is arranged on an exhaust pipe coupled to an exhaust manifold of an engine, and a filter including fine holes is arranged therein. The filter may be made of, besides metal and metal alloy, ceramic. A known example of a filter made of ceramic includes a honeycomb filter made of cordierite. Recently, a porous silicon carbide sintered material is often used as the material forming the filter because of the advantages of, for example, high thermal resistance, high mechanical strength, high collecting efficiency, chemical stability, and small pressure loss (e.g., Japanese Laid-Open Patent Publication No. 2001-162119).

The honeycomb filter has multiple cells (through-holes) extending in an axial direction thereof. When exhaust gas passes through the filter, the fine particles are trapped at the cell walls of the filter. As a result, the fine particles are removed from the exhaust gas.

However, since the honeycomb filter made of a porous silicon carbide sintered material has large thermal expansion, as the size of the filter increases, cracks tend to occur in the filter during use at high temperature. Thus, a technique for manufacturing one large ceramic filter assembly by integrating a plurality of small filter pieces has been recently proposed as a means for avoiding damage caused by cracks.

A general method for manufacturing the above mentioned assembly will now be briefly introduced.

First, a square columnar shaped honeycomb molded product is formed by continuously extruding a ceramic material through a metal mold die of an extruder. After cutting the honeycomb molded product into equal lengths, 5 each cut piece is sintered to produce a filter. After the sintering, the outer surfaces of the filters are adhered to each other by a ceramic sealing material layer to bundle and integrate the filters. Consequently, the desired ceramic filter assembly is completed. A mat thermal insulation 10 material including ceramic fibers and the like is wrapped around the outer surface of the ceramic filter assembly. The assembly in such state is accommodated within a casing arranged on the exhaust pipe.

15 [Patent Publication 1]  
Japanese Patent Publication No. 2001-162119

In case of a filter having an integrated structure and a cross section that is oblong, such as, a substantially 20 elliptical shape, it is found that cracks are more likely to occur in filters located at peripheral portions rather than at central portions of the assembly. When observing the filter assembly after repeating reproduction a number of times and dividing the filter assembly, a slight amount of 25 burnt residue of soot was found for the first time in filters located at the peripheral portions. It can thus be presumed that a temperature difference exists between individual honeycomb filters. This causes a difference in the reproduction level during a single reproducing process. 30 Further, the soot residue causes a difference in the subsequent collecting amount, and the temperature stress due to the difference in the amount of soot during reproduction causes cracks in the honeycomb filter.

## DISCLOSURE OF THE INVENTION

It is an object of the present invention to provide a ceramic filter assembly having superior strength. It is a further aspect of the present invention to provide a  
5 columnar honeycomb filter suitable for manufacturing such a ceramic filter assembly.

The inventor of the present invention has recognized  
10 that in an exhaust gas purifying device connected to an engine through a pipe having an inner diameter smaller than the filter, a temperature difference is produced between a central portion and a peripheral portion of the filter assembly when the pipe is conically enlarged just before the  
15 filter.

Further, the inventor of the present invention has recognized that in a filter assembly having an oblong shape such as substantially elliptical shape, a large temperature  
20 difference is produced between the peripheral portion in the major axis direction and the peripheral portion in the minor axis due to difference in the distance from the central portion. The inventor has confirmed that this temperature difference prevents uniform reproduction, produces residual  
25 soot, and cause cracking when the filter exceeds its strength limit.

Based on the above knowledge, the inventor has conducted tests and research to manufacture an oblong filter  
30 assembly enabling uniform temperature rise. As a result, it has become understood that if the ceramic filter assembly is manufactured so as to satisfy certain conditions, thermal stress would be absorbed and a ceramic filter assembly

having superior strength would be manufactured.

Accordingly, a conclusion has been reached that in order to uniformly transfer heat from the central portion to the peripheral portion, a condition in which the thermal conductivity in the major axis direction is higher than the thermal conductivity in the minor axis direction, particularly, a condition in which the heat insulating effect is increased at the peripheral portion of the assembly in the major axis direction compared to the peripheral portion in the minor axis direction should be satisfied.

The present inventions provides a ceramic filter assembly integrated by adhering together a plurality of columnar honeycomb filters made of a porous ceramic sintered material with a ceramic sealing material layer and having a substantially elliptical cross sectional shape when cut parallel to end faces of the plurality of honeycomb filters.

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In a first aspect, the plurality of honeycomb filters include a honeycomb filter having a rectangular cross sectional shape when cut parallel to the end faces and provided with a long side having length  $B_1$  and a short side having length  $B_2$  in which the ratio  $B_1/B_2$  is between 1.1 and 3.0. The honeycomb filter is arranged so that the long side and the short side of the honeycomb filter are respectively parallel to the major axis and minor axis of the assembly.

30 In a second aspect of the present invention, each honeycomb filter includes a plurality of rectangular cells extending along an axis of the filter with each cell provided with a long side having length  $C_1$  and a short side

having length C2 in which the ratio C1/C2 is between 1.1 and 3.0. The plurality of honeycomb filters are arranged so that the long sides of the cells are parallel to the major axis of the assembly and the short sides of the cells are parallel to the minor axis of the assembly.

In a third aspect, each honeycomb filter includes a plurality of rectangular cells extending along an axis of the filter and defined by relatively thick cell walls and relatively thin walls that are orthogonal to each other. The plurality of honeycomb filters are arranged so that the relatively thick cell walls are parallel to the major axis of the assembly and the relatively thin cell walls are parallel to the minor axis of the assembly.

In a fourth aspect, the ceramic sealing material layer includes a first sealing material layer extending parallel to the major axis of the assembly and a second sealing material layer extending orthogonal to the major axis of the assembly. The first sealing material layer is thicker than the second sealing material layer.

In a fifth aspect, the ceramic sealing material layer includes a first sealing material layer parallel to the major axis of the assembly and a second sealing material layer orthogonal to the major axis of the assembly. The first sealing material layer has a thermal conductivity lower than the thermal conductivity of the second sealing material layer.

In a sixth aspect, the ceramic filter assembly further includes an outer sealing material layer made of ceramic and formed on the periphery of the assembly. The outer sealing

material layer includes a first portion located along an extension of the major axis of the assembly that is thicker than a second portion located along an extension of the minor axis of the assembly.

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In a seventh aspect, a ceramic filter assembly integrated by adhering together a plurality of columnar honeycomb filters made of a porous ceramic sintered material with an inner sealing material layer made of ceramic and has a generally elliptical cross sectional shape when cut parallel to end faces of the plurality of honeycomb filters is provided. A tubular casing accommodates the ceramic filter assembly. A thermal insulation material is arranged between the casing and the ceramic filter assembly. The thermal insulation material includes a first portion located along an extension of the major axis of the assembly and a second portion located along an extension of the minor axis of the assembly. The first portion is thicker than the second portion.

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In an eighth aspect, a columnar honeycomb filter made of a porous ceramic sintered material is provided. The honeycomb filter has a rectangular cross sectional shape when cut parallel to an end face thereof and is provided with a long side having length B1 and a short side having length B2 in which the ratio the B1/B2 is 3.0 or less.

In a ninth aspect, the columnar honeycomb includes a plurality of cells, extending along the axial direction thereof, and an end face. Each cell has a rectangular cross sectional shape when cut parallel to the end face. Each cell is provided with a long side having length C1 and a short side having length C2 in which the ratio C1/C2 is 3.0

or less.

In a tenth aspect, a columnar honeycomb filter made of a porous ceramic sintered material includes a plurality of rectangular cells extending along the axial direction of the honeycomb filter. Each rectangular cell is defined by a relatively thick cell wall and a relatively thin cell wall that are orthogonal to each other.

In an eleventh aspect, in a ceramic filter assembly having a substantially elliptical cross sectional shape, when a hypothetical first straight line intersects the generally elliptical contour at two points in which the distance therebetween is maximum and a hypothetical second straight line orthogonal to the first straight line intersects the generally elliptical contour at two points in which the distance therebetween is maximum, the number of sealing material layers that the first straight line of the assembly traverses is less than or equal to the number of sealing material layers that the second straight line traverses.

#### BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a schematic view showing an exhaust gas purifying device including a ceramic filter assembly according to one embodiment of the present invention;

Fig. 2 is a perspective view showing the ceramic filter assembly of Fig. 1;

Fig. 3(a) is a perspective view showing a honeycomb filter having a rectangular cross section;

Fig. 3(b) is a perspective view showing a honeycomb filter having a rectangular cell;



Fig. 3(c) is a perspective view showing a honeycomb filter having a plurality of cells partitioned by cell walls that are orthogonal to each other and have different thicknesses;

5 Fig. 4 is a cross sectional view showing the exhaust gas purifying device of Fig. 1;

Figs. 5(a) to 5(e) are views showing cross sectional shapes of the ceramic filter assembly;

10 Fig. 6(a) is a side view of the filter assembly formed from a honeycomb filter having a rectangular cross section;

Figs. 6(b) and 6(c) are side views of the filter assembly formed from a honeycomb filter having a square cross section;

15 Figs. 7(a), 7(b), and 7(c) are side views of the filter assembly formed from a honeycomb filter having cells of different shapes;

Figs. 8(a), 8(b), and 8(c) are side views of a filter assembly formed from a honeycomb filter having walls of different thicknesses;

20 Figs. 9(a), 9(b), and 9(c) are side views of the filter assembly integrated with a sealing material layer of different thickness;

25 Fig. 10(a) is a side view of the filter assembly integrated by a sealing material layer of different thermal conductivity;

Fig. 10(b) is a side view of the filter assembly including an exterior sealing material layer of uneven thickness; and

30 Fig. 10(c) is a side view of the filter assembly including a thermal insulation material of uneven thickness.

## DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

An exhaust gas purifying device 1 according to one embodiment of the present invention will now be described.

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As shown in Fig. 1, the exhaust gas purifying device 1 is a device for purifying exhaust gas discharged from a diesel engine 2 serving as an internal combustion engine. The diesel engine 2 includes a plurality of cylinders (not shown). Each cylinder is connected to a branch pipe 4 of an exhaust manifold 3 that is made of a metal material. Each  
10 branch pipe 4 is connected to a single manifold body 5. Accordingly, the exhaust gas discharged from each cylinder pipe is concentrated at one location.

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A first exhaust pipe 6 and a second exhaust pipe 7 made of a metal material are arranged downstream of the exhaust manifold 3. An upstream end of the first exhaust pipe 6 is coupled to the manifold body 5. A tubular casing 8, also  
20 made of a metal material, is arranged between the first exhaust pipe 6 and the second exhaust pipe 7. An upstream end of the casing 8 is coupled to a downstream end of the first exhaust pipe 6, and a downstream end of the casing 8 is coupled to an upstream end of the second exhaust pipe 7.  
25 The exhaust gas flows through the first exhaust pipe 6, the casing 8, and the second exhaust pipe 7.

As shown in Fig. 1, a central portion of the casing 8 has a greater diameter than the exhaust pipes 6, 7. That  
30 is, the interior of the casing 8 is larger than that of the exhaust pipes 6, 7. A ceramic filter assembly 9 is accommodated in the casing 8. The exhaust gas purifying device 1 accommodating the ceramic filter assembly 9 in the

casing 8 is referred to as a canning body.

A thermal insulation material 10 is arranged between the outer surface of the assembly 9 and the inner surface of the casing 8. The thermal insulation material 10 is a mat-shaped body formed from ceramic fibers, and has a thickness of 2 mm to 60 mm. The thermal insulation material 10 preferably has an elastic structure and has a function for releasing thermal stress. The thermal insulation material 10 minimizes energy loss during reproduction by preventing heat from escaping from the outermost portion of the assembly 9. Further, due to the elastic structure, the ceramic filter assembly 9 is prevented from being displaced by the pressure of the exhaust gas and vibrations when the vehicle is traveling.

The ceramic filter assembly 9 of the present embodiment is for removing diesel particulates as mentioned above, and is thus normally referred to as a diesel particulate filter (DPF). As shown in Fig. 2 and Fig. 4, the assembly 9 of the present embodiment is formed by bundling and integrating a plurality of honeycomb filters F1. Among the plurality of honeycomb filters F1, the honeycomb filters F1 located at the central portion of the assembly 9 each has a square columnar shape, as shown in Figs. 3(a) to 3(C). Honeycomb filters F1 having a shape other than a square columnar shape are arranged around the square columnar shaped honeycomb filters F1. As a result, when seen as a whole, the ceramic filter assembly 9 has a substantially elliptic cylinder shape with a substantially elliptical cross sectional shape.

The cross section of the assembly 9 of the present invention is substantially elliptical. "Substantially

elliptical" is not limited only to an ellipse configured only by curves, as shown in Fig. 5(a). An oblong elliptical shape partially having, for example, straight lines as shown in Fig. 5(b), more specifically, a pair of straight parallel lines to each other is also included. The straight portion may only be at one section, or may be at more than three sections. "Oblong" includes shapes as shown in Fig. 5(a), Fig. 5(b), Fig. 5(c), Fig. 5(d), and Fig. 5(e). The lengths of the major axis and minor axis of the assembly 9 are defined as A1 and A2 ( $A1 > A2$ ), respectively. If the substantially elliptical shape is an ellipse, a long axis passing a focal point is the major axis, and a short axis orthogonal thereto is the minor axis. The dimensions A1 and A2 are preferably 500 mm or less. If the dimensions A1 and A2 are greater than 500 mm, it becomes difficult to manufacture the assembly with sufficient strength.

The length L (mm) of each honeycomb filter F1 is defined as the dimension of the direction in which the exhaust gas or fluid subjected to treatment flows (direction orthogonal to the end face of the filter). When each honeycomb filter F1 is cut perpendicular to the flow direction of the exhaust gas (that is, cut parallel to the end face of the filter), the cross section is rectangular. The lengths (outside dimension) of the long side and the short side of the cross section of the honeycomb filter F1 are defined as B1 and B2 ( $B1 \geq B2$ ), respectively. Each of the dimensions B1 and B2 are preferably 110 mm or less. This is because the strength of the filter F1 decreases significantly when the dimensions B1 and B2 are greater than 110 mm.

It is preferred that the ratio of  $B1/B2$  be 3 or less.

This is because if the ratio of B1/B2 is greater than 3, thermal stress is more likely to act on the filter F1 due to thermal shock, and cracks are more likely to occur.

5       The honeycomb filter F1 is made of a porous silicon carbide sintered material, which is one type of porous ceramic sintered material. The silicon carbide sintered material is used because of its excellent thermal resistance and heat conductivity when compared to other ceramics.  
10       Instead of silicon carbide, the sintered material may be made of, for example, silicon nitride, sialon, alumina, cordierite, mullite, and the like.

      Silicic ceramics in which metal silicon is mixed to the  
15       above mentioned ceramic, and ceramics bonded with silicon and silicate compound may also be used. This is because the metal silicon prevents cracks caused by thermal shock and the like.

20       It is preferred that 5 to 50 parts by weight of metal silicon is included per 100 parts by weight of silicon carbide. If the amount of metal silicon is too small, the adhesive strength of the filter F1 decreases, and if the amount is too large, the filter F1 becomes dense and the  
25       properties necessary as the filter cannot be obtained.

      As shown in, for example, Fig. 3(a) to Fig. 3(c), each honeycomb filter F1 has a so-called honeycomb structure. The honeycomb structure is adopted because the pressure loss  
30       is small even if the collected amount of fine particles increases. Each honeycomb filter F1 includes a plurality of cells 12 (through-holes) having a rectangular cross section, regularly formed in the axial direction thereof. The

lengths of the sides (inner diameter) of the rectangular cross section of each cell 12 are defined as  $C_1$  and  $C_2$  ( $C_1 \geq C_2$ ). The cells 12 are partitioned from each other by thin cell walls 13a and 13b. The thickness of the cell walls 13a, 13b are defined as  $D_1$  and  $D_2$  ( $D_1 \geq D_2$ ), respectively.

The ratio  $C_1/C_2$  is preferably 3 or less. This is because if the ratio  $C_1/C_2$  is greater than 3, thermal stress is more likely to act on the filter F1 due to thermal shock, and cracks are more likely to occur.

The ratio  $D_1/D_2$  is preferably 3 or less. This is because if the ratio  $D_1/D_2$  is greater than 3, thermal stress is more likely to act on the filter F1 due to thermal shock, and cracks are more likely to occur.

An oxidation catalyst made of platinum group elements (e.g., Pt) and other metal elements and oxides thereof are carried by the cell walls 13a and 13b. Each cell 12 is sealed with a plug 14 (made of a porous silicon carbide sintered material in this embodiment) at either one of the end faces  $9\alpha$  and  $9\beta$  of the filter F1. A checker-board like pattern is formed on the end faces  $9\alpha$  and  $9\beta$  by the sealed cells 12. The density of the cell 12 is preferably approximately 200 cells/square inch. About half of the cells 12 are open at the upstream side end face  $9\alpha$  and the remaining cells 12 are open at the downstream side end face  $9\beta$ . The lengths  $C_1$ ,  $C_2$  of the sides of the cell 12 are preferably set between 0.5 mm and 5.0 mm. If the dimensions  $C_1$ ,  $C_2$  are greater than 5.0 mm, the filtering surface area of the cell walls 13a and 13b becomes small. This lowers the performance of the filter F1. On the other hand, if the

dimensions C1 and C2 are smaller than 0.5 mm, the filter F1 becomes very difficult to manufacture. The thicknesses D1, D2 of the cell walls 13a, 13b are preferably set between 0.1 to 0.5 mm. This is because if the dimensions D1 and D2 are greater than 0.5 mm, the fluid resistance (pressure loss) produced by the filter F1 becomes high and is thus not satisfactory. If, on the other hand, the dimensions D1 and D2 are smaller than 0.1 mm, the strength of the filter F1 becomes insufficient.

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The average pore diameter of the honeycomb filter F1 is preferably between  $1\mu\text{m}$  and  $50\mu\text{m}$ , and more preferably, between  $5\mu\text{m}$  and  $20\mu\text{m}$ . If the average pore diameter is less than  $1\mu\text{m}$ , the honeycomb filter F1 would often become clogged by the deposition of fine particles. If, on the other hand, the average pore diameter exceeds  $50\mu\text{m}$ , small fine particles cannot be collected. This would reduce the collecting efficiency.

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The porosity of the honeycomb filter F1 is preferably between 30% and 80%, and more preferably, between 40% and 60%. If the porosity is less than 30%, the honeycomb filter F1 becomes too dense and may not allow the passage of exhaust gas. If the porosity exceeds 80%, the amount of gaps formed in the honeycomb filter F1 becomes excessive. This would weaken the strength and decrease the collecting efficiency of the fine particles.

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When a porous silicon carbide sintered material is selected, the thermal conductivity of the honeycomb filter F1 is preferably between  $5\text{W/m}\cdot\text{K}$  and  $80\text{W/m}\cdot\text{K}$ , and more preferably, between  $30\text{W/m}\cdot\text{K}$  and  $70\text{W/m}\cdot\text{K}$ .

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As shown in Fig. 2, Fig. 4, and Fig. 10(a), the outer surfaces of the honeycomb filters F1 are adhered to each other by means of ceramic sealing material layers 15a and 15b. The ceramic sealing material layers 15a and 15b are defined to be of the same type for those that are parallel to each other. Hereinafter, the ceramic sealing material layers parallel to the long side of the assembly 9 are denoted by 15a, the thickness of which is  $E1$ , the thermal conductivity of which is  $G1$ . The ceramic sealing material layers parallel to the short side of the assembly 9 is denoted by 15b, the thickness of which is  $E2$  ( $E1 \geq E2$ ), and the thermal conductivity of which is  $G2$ . The ratio of  $E1/E2$  is preferably equal to or less than 5. If the ratio  $E1/E2$  is greater than 5, the heat conduction reverses between the short side direction and the long side direction, and thus a uniform temperature rise of the assembly 9 becomes difficult. The ratio  $E1/E2$  is preferably 1.05 or greater. If the ratio  $E1/E2$  is less than 1.05, thermal conduction in the direction of the long side becomes difficult. Thus, uniform temperature rise of the assembly 9 becomes difficult. This produces soot and cracks become likely to occur.

If the thicknesses of the sealing material layers 15a and 15b are the same, the thermal conductivity  $G1$  and  $G2$  of both sealing material layers 15a and 15b may be adjusted by differing the compositions (compound) of the sealing material layers 15a and 15b from each other. In this case, the ratio  $G1/G2$  is preferably 0.20 or greater. If the ratio  $G1/G2$  is smaller than 0.20, the thermal conduction reverses between the short side direction and the long side direction, and thus a uniform temperature rise of the assembly 9 becomes difficult. The ratio  $G1/G2$  is preferably



0.7 or less. If the ratio  $G1/G2$  is greater than 0.7, the thermal conduction in the direction of the long side becomes difficult. This produces soot and cracks become likely to occur.

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The ceramic sealing material layers 15a, 15b of the present invention will now be described in detail.

The thicknesses E1 and E2 of the sealing material layers 15a and 15b are preferably between 0.3 mm and 3 mm, and more preferably between 0.5 mm and 2 mm. If the thicknesses E1 and E2 exceed 3 mm, the thermal resistance of the sealing material layers 15a and 15b become large even if the thermal conductivity is high, thus inhibiting the thermal conduction between the honeycomb filters F1. The percentage of the honeycomb filters F1 occupying the assembly 9 also relatively decreases, thus leading to lower filtering performance. If, on the other hand, the thicknesses E1 and E2 of the sealing material layers 15a and 15b are less than 0.3 mm, the thermal resistance will not be large but the force adhering the honeycomb filters F1 to each other becomes insufficient, and thus the assembly 9 is likely to break.

The sealing material layers 15a and 15b include at least inorganic fibers, an inorganic binder, an organic binder, and inorganic particles. Further, the sealing material layers 15a and 15b preferably made of an elastic material formed by bonding the inorganic fibers and the inorganic particles with the inorganic binder and the organic binder.

The inorganic fiber contained in the sealing material

layers 15a and 15b include at least one or more types of ceramic fiber selected from silica-alumina fiber, mullite fiber, alumina fiber, and silica fiber. Among these fibers, silica-alumina ceramic fiber is particularly preferable.

- 5 This is because silica-alumina ceramic fiber has excellent elasticity and exhibits thermal stress absorbing performance.

10 The content of the silica-alumina ceramic fiber in the sealing material layers 15a and 15b is 10% by weight to 70% by weight, preferably 10% by weight to 40% by weight, and more preferably, 20% by weight to 30% by weight in solid content. If the content of the silica-alumina ceramic fiber is less than 10% by weight in the solid content, the effect  
15 as an elastic body decreases. If the content of the silica-alumina ceramic fiber exceeds 70% by weight, not only does the thermal conductivity decrease, but elasticity also decreases.

20 Shot content in the silica-alumina ceramic fiber is 1% by weight to 10% by weight, preferably 1% by weight to 5% by weight, and more preferably, 1% by weight to 3%. If the shot content is less than 1% by weight, manufacturing becomes difficult. If, on the other hand, the shot content  
25 exceeds 50% by weight, the outer surface of the honeycomb filter F1 tends to be damaged.

The fiber length of the silica-alumina ceramic fiber is 1  $\mu\text{m}$  to 100 mm, preferably, 1  $\mu\text{m}$  to 50 mm, and more  
30 preferably, 1  $\mu\text{m}$  to 20 mm. If the fiber length is shorter than 1  $\mu\text{m}$ , an elastic structure cannot be formed. If the fiber length exceeds 100 mm, fuzzballs of fibers are formed. This lowers dispersion of the inorganic fine particles.

Further, it becomes difficult to make the sealing material layers 15a and 15b less than or equal to 3 mm, and the thermal conductivity between the honeycomb filters F1 cannot be improved.

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The inorganic binder contained in the sealing material layers 15a and 15b is preferably at least one or more types of colloidal sol selected from silica sol and alumina sol.

Among these sols, silica sol is particularly preferable.

10 This is because silica sol is easy to obtain, easily becomes  $\text{SiO}_2$  by performing sintering, and is thus suitable as an adhesive agent under high temperatures. Furthermore, silica sol has superior insulation.

15 The content of the silica sol in the sealing material layers 15a and 15b is 1% by weight to 30% by weight, preferably, 1% by weight to 15% by weight, and more preferably, 5% by weight to 9% by weight in solid content. If the content of the silica sol is less than 1% by weight,  
20 the adhesion strength decreases. If the content of the silica sol exceeds 30% by weight, this may reduce thermal conductivity.

The organic binder contained in the sealing material  
25 layers 15a and 15b is preferably a hydrophilic organic macromolecule, and more preferably, at least one or more types of polysaccharide selected from polyvinyl alcohol, methyl cellulose, ethyl cellulose, and carboxymethyl cellulose. Among these, carboxymethyl cellulose is  
30 particularly preferable. This is because carboxymethyl cellulose produces suitable fluidity for the sealing material layers 15a and 15b and thus exhibits excellent adhesiveness under normal temperatures.

The content of the carboxymethyl cellulose in the sealing material layers 15a and 15b is 0.1% by weight to 5.0% by weight, preferably, 0.2% by weight to 1.0% by weight, and more preferably, 0.4% by weight to 0.6% by weight in solid content. If the content of the carboxymethyl cellulose is less than 0.1% by weight, migration can not be sufficiently suppressed. "Migration" is a phenomenon in which the binder in the sealing material layers 15a and 15b migrates as the solvent is dried and removed when the sealing material layers 15a and 15b filled between the subjected sealing body cure. If the content of the carboxymethyl cellulose exceeds 5% by weight, the organic binder is burnt by the high temperature and the strength of the sealing material layers 15a and 15b is lowered.

The inorganic particles contained in the sealing material layers 15a and 15b is preferably an elastic material using a whisker or at least one or more types of inorganic powder selected from silicon carbide, silicon nitride, and boron nitride. Such carbides and nitrides have very large thermal conductivities, and are arranged on the ceramic fiber surface or on the surface and the inside of the colloidal sol and contribute to the enhancement of thermal conduction.

Among the inorganic particles of the above carbides and nitrides, silicon carbide powder is particularly preferable. This is because silicon carbide has an extremely high thermal conductivity, and in addition, has affinity for ceramic fiber. Moreover, this is because the honeycomb filter F1 serving as the subjected sealing body is of the same type, in other words, is made of porous silicon carbide

in the present embodiment.

The content of silicon carbide powder is 3% by weight to 80% by weight, preferably, 10% by weight to 60% by weight, and more preferably, 20% by weight to 40% by weight in solid content. If the content of the silicon carbide powder is less than 3% by weight, the thermal conductivity of the sealing material layers 15a and 15b decreases and causes the sealing material layers 15a and 15b to remain as a large thermal resistance. If, on the other hand, the content exceeds 80% by weight, the adhesion strength under a high temperature decreases.

The particle diameter of the silicon carbide powder is between 0.01  $\mu\text{m}$  and 100  $\mu\text{m}$ , preferably, between 0.1  $\mu\text{m}$  and 15  $\mu\text{m}$ , and more preferably between 0.1  $\mu\text{m}$  and 10  $\mu\text{m}$ . If the particle diameter exceeds 100  $\mu\text{m}$ , the adhesive force and thermal conductivity decrease. If the particle diameter is less than 0.01  $\mu\text{m}$ , the cost of the sealing material layers 15a and 15b increases.

The procedures for manufacturing the above mentioned ceramic filter assembly 9 will now be described.

First, a ceramic ingredient slurry used in an extrusion molding process, a sealing paste used in an end face sealing process, and a sealing material layer forming paste used in a filter adhesion process are prepared in advance.

The ceramic ingredient slurry is formed by mixing and kneading a predetermined amount of silicon carbide powder, organic binder, and water (in some cases, metal silicon is also added). The sealing paste is formed by mixing and

kneading silicon carbide powder, organic binder, lubricant, plasticizer, and water. The sealing material layer forming paste is formed by mixing and kneading predetermined amounts of inorganic fibers, inorganic binder, organic binder,  
5 inorganic particles, and water.

Next, the ceramic ingredient slurry is charged into the extruder, and is continuously extruded through a metal mold die. The extruded honeycomb molded product is cut into  
10 equal lengths to obtain cut pieces of square columnar honeycomb molded products. Further, a predetermined amount of sealing paste is filled into an opening on one side of each cell of the cut piece to seal both end faces of each cut piece.

15 Subsequently, sintering temperature, sintering time and the like are set to a predetermined condition to perform main sintering, and the honeycomb molded product cut piece and the plug 14 are completely sintered. To have the  
20 average pore diameter be 6  $\mu\text{m}$  to 100  $\mu\text{m}$ , and the porosity be 30% to 80%, the sintering temperature is set to 1400°C to 2300°C in the present embodiment. The sintering time is set between 0.1 hour and 5 hours. The atmosphere within the furnace during sintering is inactive, and the pressure of  
25 the atmosphere is normal.

Next, after a base coating layer made of ceramic is formed on the outer surface of the honeycomb filter F1 if necessary, the sealing material layer forming paste is  
30 applied thereto. Then, 4 to 130 of such honeycomb filters F1 are used to adhere the outer surfaces of the honeycomb filters F1 with each other and integrate the honeycomb filters F1.

In the subsequent outer shape cutting process, unnecessary parts of the peripheral portion of the assembly 9 having a square cross section obtained through the filter adhering process is ground and removed, the ceramic sealing material layer forming paste is applied to the peripheral portion to form an outer ceramic sealing material layer. This adjusts the outer shape. As a result, the ceramic filter assembly 9 having a substantially elliptical cross section is manufactured.

The outer ceramic sealing material layer will now be described. The thickness of a normal outer ceramic sealing material layer is uniform. In the present embodiment, as shown in Fig. 10(b), in the outer ceramic sealing material layer, the portion contacting the long side of the assembly 9 is denoted by 15c, the portion contacting the short side of the assembly 9 is defined as 15d, and the thickness of portion 15c is denoted by H1, and the thickness of portion 15d is denoted by H2.

Depending on the type of assembly 9, the cell 12, or recesses, are exposed from the peripheral surface of the assembly 9 by the grinding process. In this case, the thickness of the ceramic sealing material layer is defined as the distance from a curve surface connecting the cell walls 13a and 13b of the exposed cells 12.

The ceramic sealing material layer forming paste is applied so that the thickness of the middle part between the portion 15c and the portion 15d changes gradually. The adjustment of the thickness of the ceramic sealing material layer is possible by performing machining after the application of the paste. Alternatively, the sealing

material layer may be formed by injecting and drying the ceramic sealing material in the mold so that the sealing material layer has such thickness.

5       The ratio  $H2/H1$  is preferably 0.95 or less. If the ratio  $H2/H1$  is greater than 0.95, the filter in the long side direction easily cools, and uniform temperature rise of the assembly 9 becomes difficult. This causes soot to remain and cracks tend to occur.

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      The ratio  $H2/H1$  is preferably 0.06 or greater. If the ratio  $H2/H1$  is less than 0.06, the release of heat reverses between the short side direction and the long side direction. Thus, a uniform temperature rise of the assembly 9 becomes difficult.

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      The assembly 9 is wrapped by the thermal insulation material 10 (refer to Fig. 1 and Fig. 10(c)) and is accommodated in the casing 8. The thermal insulation material normally has a uniform thickness. In the present embodiment, the thickness of the thermal insulation material differs between portion 16a, which contacts the long side of the assembly 9, and portion 16b, which contacts the short side of the assembly 9. In the following description, the thickness of portion 16a is denoted by  $I1$ , and the thickness of portion 16b is denoted by  $I2$ .

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      The ratio of  $I2/I1$  is preferably 0.91 or less. If the ratio  $I2/I1$  is greater than 0.91, the filters  $F1$  near the outer side in the direction of the long side cools easily, uniform temperature rise of the assembly 9 becomes difficult, and soot remains thereby causing cracks to easily occur. It is preferable that the ratio  $I2/I1$  be 0.30 or

30



greater. If the ratio  $I_2/I_1$  is less than 0.30, the heat release reverses between the short side direction and the long side direction and thus uniform temperature rise of the assembly 9 becomes difficult.

5

For the thermal insulation material 10, a mat formed from typical ceramic fibers, alumina fibers, and alumina silicate fibers may be used.

10        The fine particle trapping effect of the ceramic filter assembly 9 will now be briefly described.

Exhaust gas, which is supplied from the upstream side end face  $9\alpha$  of the ceramic filter assembly 9, flows into the  
15 cells 12 that are opened in the upstream side end face  $9\alpha$ . The exhaust gas passes through the cell walls 13a and 13b and reaches the interior of the cells 12 opened in the adjacent downstream end face  $9\beta$ . The gas that passes through the walls 13a and 13b flows out from the downstream side end  
20 face  $9\beta$  of the honeycomb filter F1 through the opening of the corresponding cells 12. The fine particles contained in the exhaust gas does not pass through the cell walls 13a and 13b and become trapped in the walls 13a and 13b. And, the gas from which the fine particles are removed (purified gas)  
25 is discharged from the downstream side end face  $9\beta$  of the honeycomb filter F1. The purified gas passes through the second exhaust pipe 7 and is released into the atmosphere. The trapped fine particles are ignited and burned by the action of the above mentioned catalyst when the internal  
30 temperature of the assembly 9 reaches a predetermined temperature.

A thermal shock test conducted on the filter will now

be described.

[Test 1]

5 First, 51.5% by weight of  $\alpha$ -silicon carbide powder having an average particle diameter of 10  $\mu\text{m}$  and 22% by weight of  $\beta$ -silicon carbide powder having an average particle diameter of 0.5  $\mu\text{m}$  were wet mixed, and 6.5% by weight of organic binder (methyl cellulose) and 20% by  
10 weight of water were added to the obtained mixture and kneaded. Next, a small amount of plasticizer and lubricant were added to the kneaded mixture and was further kneaded, and was then extruded with a different metal mold die to obtain a honeycomb molded product.

15 Subsequently, after drying the molded product with a microwave drier, the cells (through holes) of the molded product were sealed with the sealing paste made of a porous silicon carbide sintered material. Then, the drier was used  
20 again to dry the sealing paste. Subsequently, the dried body was degreased at 400°C, and then baked for about 3 hours at 2200°C under an argon atmosphere of normal pressure. As a result, a honeycomb filter F1 made of porous silicon carbide sintered body was obtained. In accordance  
25 with this method, a filter having a dimension as shown in table 1 was prepared. The length of each filter was unified to 150 mm.

Each filter was gradually heated to 600°C or 800°C in an  
30 electric furnace, and was held for 3 hours at a target temperature. Thereafter, the filter was placed under a normal temperature of 20°C to apply thermal shock to the

filter. The occurrence of cracks is shown in table 1.

With the thermal shock of 600°C and 800°C, cracks occurred when the ratio B1/B2 was 3.04 or greater. It was found that a filter can sufficiently withstand a thermal shock of about 800°C, at which it may be used, when the ratio B1/B2 is 3.0 or less.

[Test 2]

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First, 51.5% by weight of silicon carbide powder having an average particle diameter 10  $\mu\text{m}$ , 12% by weight of silicon carbide powder having an average particle diameter of 0.5  $\mu\text{m}$ , and 10% by weight of metal silicon having an average particle diameter of 0.5  $\mu\text{m}$  were wet mixed, and 6.5% by weight and 20% by weight of the organic binder (methyl cellulose) and water were each added to the obtained mixture and kneaded. Next, a small amount of plasticizer and lubricant were added to the kneaded mixture and was further kneaded, and was then extruded with a different metal mold die to obtain a honeycomb molded product.

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Subsequently, after drying the molded product with a microwave drier, the cells (through holes) of the molded product were sealed with the sealing paste made of a porous silicon carbide sintered material. The drier was used again to dry the sealing paste. Subsequently, the dried body was degreased at 400°C, and then baked for about 3 hours at 1500°C under an argon atmosphere of normal pressure. As a result, a honeycomb filter F1 made of porous silicon carbide - metal silicon sintered material was obtained. In accordance with this method, filters having the dimensions

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shown in table 2 were prepared. The length of each filter was unified to 150 mm. In the same manner as test 1, a thermal shock test was conducted. As shown in table 2, with a thermal shock of 600°C, cracks occurred when the ratio B1/B2 was 3.09 or greater. In the thermal shock of 800°C, cracks occurred when the ratio B1/B2 was 3.04 or greater. It was found that a filter can sufficiently withstand a thermal shock of about 800°C, at which it is used, when the ratio B1/B2 is 3.0 or less.

#### [Test 3]

In test 3, filters were manufactured through the same procedure as in test 1. However, the inner diameter of the cells (through holes) was changed. The result of the dimensions and the thermal shock test is shown in table 3. It is apparent from the result that with a thermal shock of 600°C and 800°C, cracks occurred when the ratio C1/C2 was 3.07 or greater. It was found that a filter can sufficiently withstand a thermal shock of about 800°C, at which it is used, when the ratio C1/C2 is equal 3.0 or less.

#### [Test 4]

In test 4, filters were manufactured through the same procedure as in test 2. However, the inner diameter of the cells (through holes) was changed. The result of the dimensions and the thermal shock test is shown in table 4. It is apparent from the result that with a thermal shock of 600°C, cracks occurred when the ratio C1/C2 was 3.20 or greater, and with a thermal shock of 800°C, cracks occurred when the ratio C1/C2 was 3.07 or greater. It was found that

a filter can sufficiently withstand a thermal shock of about 800°C, at which it is used, when the ratio  $C1/C2$  is 3.0 or less.

5 [Test 5]

In test 5, filters were manufactured through the same procedure as in test 1. However, the wall thickness was changed. The result of the dimensions and the thermal shock  
10 test is shown in table 5. It is apparent from the result that with thermal shock of 600°C and 800°C, cracks occurred when the ratio  $D1/D2$  was 3.03 or greater. It was found that a filter can sufficiently withstand the thermal shock of about 800°C, at which it is used, when the ratio  $D1/D2$  is  
15 3.0 or less.

[Test 6]

In test 6, filters were manufactured through the same  
20 procedure as in test 2. However, the wall thickness was changed. The dimensions and the results of the thermal shock are shown in table 6. It is apparent from the results that with thermal shock of 600°C, cracks occurred when the ratio  $D1/D2$  was 3.08 or greater, and with thermal shock of  
25 800°C, cracks occurred when the ratio  $D1/D2$  was 3.03 or greater. It was found that a filter can sufficiently withstand a thermal shock of about 800°C, at which it is used, when the ratio  $D1/D2$  is 3.0 or less.

30 EXAMPLES AND COMPARATIVE EXAMPLES

(Example 1-1)

First, 51.5% by weight of  $\alpha$ -silicon carbide powder and 22% by weight of  $\beta$ -silicon carbide powder were wet mixed, and 6.5% by weight of an organic binder (methyl cellulose) and 20% by weight of water were added to the obtained  
5 mixture and kneaded. Next, a small amount of plasticizer and lubricant were added to the kneaded mixture and was further kneaded, and was then extruded with a different metal mold die to obtain a honeycomb molded product.

10 Subsequently, after drying the molded product with a microwave drier, the cells (through holes) 12 of the molded product were sealed with the sealing paste made of a porous silicon carbide sintered material. Then, the drier was used again to dry the sealing paste. Subsequently, the dried  
15 body was degreased at 400°C, and was then baked for about 3 hours at 2200°C under an argon atmosphere at normal pressure. As a result, honeycomb filters F1 made from the porous silicon carbide sintered material were obtained. In each honeycomb filter, the long side B1 was set to 66.9 mm,  
20 the short side B2 was set to 32.7 mm, the length L was set to 150 mm, both lengths of the long side and the short side of the cells 12 were set to 1.5 mm, and both thicknesses D1 and D2 of the cell walls 13a and 13b were set to 0.3 mm (in the same manner as in test example 1.2).

25 Then, 23.3% by weight of ceramic fibers, 30.2% by weight of silicon carbide powder having an average particle diameter of 0.3  $\mu$ m, 7% by weight of silica sol serving as the inorganic binder, 0.5% by weight of carboxymethyl  
30 cellulose serving as the inorganic binder, and 39% by weight of water were mixed and kneaded. By adjusting such kneaded mixture to an appropriate viscosity, the paste used for forming the sealing material layers 15a, 15b, and 15c was

prepared. The ceramic fibers were alumina silicate ceramic fibers having a shot content of 3% with fiber lengths of 0.1 mm to 100 mm, and the conversion amount of silica sol in terms of  $\text{SiO}_2$  amount was 30%.

5

The sealing material layer forming paste was then uniformly applied to the outer surfaces of the honeycomb filters F1 to form the sealing material layers 15a and 15b with a thickness of 1.0 mm. Nine honeycomb filters F1 were arranged in the same direction in three rows and three columns and dried for 1 hour at 100 °C with the outer surfaces adhered to each other. The sealing material layers 15a and 15b were then cured, and the nine honeycomb filters F1 were integrated. The outer shape cutting process was performed to form an ellipse with the cross sectional shape of the assembly of the integrated nine honeycomb filters F1. The major axis A1 of the ellipse was 160 mm, the minor axis A2 was 80 mm, and the ratio A1/A2 was 2. The sealing material layer 15c having a thickness of 1.5 mm was applied to the peripheral portion of the assembly and the outer shape was cut and trimmed to manufacture a ceramic filter assembly 9a having a substantially elliptical cross section, as shown in Fig. 6(a).

25 The thermal insulation material 10 was uniformly wrapped around the assembly 9a that was obtained as described above to a thickness of 10 mm. The assembly 9a was accommodated in the casing 8, and the exhaust gas was actually supplied. As shown in Fig. 3(a), a thermocouple was embedded at one location P(Temp.) at substantially the center of the honeycomb filter F1, and the temperatures  $T_\alpha$ ,  $T_\beta$ , and  $T_\gamma$  of the honeycomb filter F1 at three locations denoted by  $\alpha$ ,  $\beta$ , and  $\gamma$  in Fig. 6(a) were measured with time.

$T_\alpha$  is the temperature at the center of a filter,  $T_\beta$  is the temperature at a position 5 mm from the outermost surface of the filter in the direction of the minor axis, and  $T_\gamma$  is the temperature 5 mm from the outermost surface of the filter in the direction of the major axis. The maximum temperature differences  $\Delta T$  ( $^{\circ}\text{C}$ ) between the positions  $\alpha$ ,  $\beta$ , and  $\gamma$  were also measured. The black arrow in Fig. 3 shows the direction of the flow of the exhaust gas.

After repeating the reproduction test for a number of times (10 times), the assembly 9 was taken out and each honeycomb filter F1 was visually observed to study the residual soot and the occurrence of cracks. As a result, in example 1, the maximum temperature difference  $\Delta T$  ( $^{\circ}\text{C}$ ) was approximately  $50^{\circ}\text{C}$ , the value of which is extremely small. Further, no residual soot was present in any of the honeycomb filters F1, and the occurrence of cracks was not confirmed.

(Comparative examples 1-1 to 1-2)

In comparative examples 1-1 and 1-2, the assembly 9 was manufactured basically in the same manner as in example 1-1. However, in comparative example 1-1, the long side B1 of each honeycomb filter F1 was changed to 32.7 mm, the short side B2 was changed to 32.7 mm, and the length L was changed to 150 mm (in the same manner as in test reference example 1.1 (table 1)). Nine filters were arranged in three rows and three columns with the long side B1 parallel to each other to manufacture the assembly 9b with a circular cross section of diameter 80 mm, as shown in Fig. 6(b). In comparative example 1-2, the long side B1 of each honeycomb filter F1 was changed to 32.7 mm, the short side B2 was



changed to 32.7 mm, and the length L was changed to 150 mm (in the same manner as in test reference example 1.1 (table 1). Fifteen filters were arranged in three rows and five columns with the long side B1 parallel to each other to manufacture assembly 9c with a substantially elliptical cross section (160 mm x 80 mm), as shown in Fig. 6(c).

The same test as in example 1-1 was performed on the two types of assemblies 9b and 9c. As a result, in comparative example 1-1, the maximum temperature difference  $\Delta T(^{\circ}\text{C})$  was about  $50^{\circ}\text{C}$ , which value is an extremely small value. No residual soot was present in any of the honeycomb filters F1, the occurrence of cracks was not confirmed.

However, in comparative example 1-2,  $\Delta T$  was approximately  $100^{\circ}\text{C}$ , the value of which is very large. Further, residual soot was present and the occurrence of cracks was confirmed in the honeycomb filter F1 located at position  $\gamma$ .

In the same manner, a similar test was performed on the silicon carbide - metal silicon filter with respect to the maximum temperature difference  $\Delta T(^{\circ}\text{C})$  and the occurrence of cracks.

More specifically, in example 1-2, the assembly in which the filters of test example 2.2 (table 2) were assembled as shown in Fig. 6(a) was used. In comparative example 1-3, the assembly in which the filters of test comparative example 2.1 were assembled as shown in Fig. 6(b) was used. In comparative example 1-4, the assembly in which the filters of test comparative example 2.1 were assembled as shown in Fig. 6(c) was used.

As shown in table 7, the maximum temperature difference  $\Delta T(^{\circ}\text{C})$  was  $60^{\circ}\text{C}$  in example 1-2, whereas in comparative example 1-4, the temperature difference was  $110^{\circ}\text{C}$  or greater, and cracks were conformed in the honeycomb filter at position  $\gamma$ .

(Examples 2-1 to 2-4)

In examples 2-1 to 2-4, the assembly 9 was manufactured basically in the same manner as in comparative examples 1-3. In example 2-1, in the cells 12 of each honeycomb filter F1, C1 was set to 1.7 mm and C2 was set to 1.5 mm. Therefore,  $C1/C2=1.13$ . Five honeycomb filters F1 were arranged parallel to the long side of the cell 12, and three honeycomb filters F1 were arranged perpendicular to the long side of the cells 12 to assemble an assembly of fifteen honeycomb filters F1. The outer shape cutting process was performed to manufacture an assembly 9d (160 mm  $\times$  80 mm  $\times$  150 mm) having a substantially elliptical cross section, as shown in Fig. 7(a). As shown in table 8, examples 2-2 to 2-4 differ from example 2-1 only in the dimensions of the cells 12.

(Comparative examples 2-1 to 2-4)

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The assembly 9 was also manufactured basically in the same manner as in example 2-1 in comparative examples 2-1 to 2-4. However, in comparative example 2-1, the dimension C1 of the cell 12 was 1.5 mm, C2 was 1.5 mm, and  $C1/C2=1$ . After assembling the honeycomb filters F1 in three rows and five columns, the outer shape cutting was performed to manufacture an assembly 9e (160 mm  $\times$  80 mm  $\times$  150 mm) having a substantially elliptical cross section, as shown in Fig.

7(b). In comparative example 2-2, the dimension C1 of the cell 12 was 1.5 mm, C2 was 1.7 mm, and  $C1/C2=0.88$ . Fifteen honeycomb filters F1 were assembled by arranging five sets of the filters F1 parallel to the 1.5 mm side with three  
5 filters F1 arranged vertically in each set. The outer shape cutting was performed to manufacture assembly 9f (160 mm × 80 mm × 150 mm) having a substantially elliptical cross section, as shown in Fig. 7(c). The comparative example 2-3  
10 example 2-2, and comparative example 2-4 was manufactured in the same manner as in example 2-1.

With respect to the assemblies of examples 2-1 to 2-4, and comparative examples 2-1 to 2-4, the maximum temperature  
15 difference  $\Delta T$  and the occurrence of cracks were studied. As a result, the maximum temperature difference  $\Delta T$  ( $^{\circ}\text{C}$ ) was  $93^{\circ}\text{C}$  or less in examples 2-1 to 2-4, and no residual soot was present in any of the honeycomb filters F1, and the occurrence of cracks was not confirmed.

20 However, in comparative example 2-1, comparative example 2-2, and comparative example 2-3, the maximum temperature difference  $\Delta T$  ( $^{\circ}\text{C}$ ) was greater than or equal to  $100^{\circ}\text{C}$ , the value of which is very large. Residual soot was  
25 present and the occurrence of cracks was confirmed in the honeycomb filter F1 at position  $\gamma$ . Further, in comparative example 2-4, the temperature difference was low but cracks occurred.

30 (Examples 2-5 to 2-8, comparative examples 2-5 to 2-8)

In the same manner, the maximum temperature difference

$\Delta T$  ( $^{\circ}\text{C}$ ) and the occurrence of cracks in the silicon carbide - metal silicon filter were studied.

More specifically, in examples 2-5 to 2-8, the filters of test examples 4.1 to 4.4 (table 4) were used in a state assembled as shown in the assembly of Fig. 7(a). In comparative example 2-5, the filters of the test reference example 4.1 were used in a state assembled as shown in Fig. 7(b). In comparative examples 2-6, 2-7, the filters of test examples 4.1 and 4.2, were used in a state assembled as shown in the assembly of Fig. 7(c). In comparative example 2-8, the filters of test comparative example 4.1 were used in a state assembled as shown in the assembly of Fig. 7(a).

The maximum temperature difference  $\Delta T$  ( $^{\circ}\text{C}$ ) of examples 2-5 to 2-8 was  $110^{\circ}\text{C}$  or less, whereas the maximum temperature difference  $\Delta T$  ( $^{\circ}\text{C}$ ) of comparative examples 2-5 to 2-8 was  $110^{\circ}\text{C}$  or greater, and cracks occurred in the honeycomb filter located at position  $\gamma$ .

The results are shown in table 8.

(Examples 3-1 to 3-4)

In examples 3-1 to 3-4, the assembly 9 was manufactured basically in the same manner as in comparative example 1-3. However, in example 3-1, the dimension  $D1$  of the cell wall 13 of each honeycomb filter  $F1$  was changed to  $0.4\text{mm}$ , and  $D2$  was changed to  $0.35\text{ mm}$ . Therefore,  $D1/D2=1.14$ . Five honeycomb filters  $F1$  were arranged parallel to  $D1$  and three honeycomb filters  $F1$  were arranged perpendicular to  $D1$  to form an assembly of fifteen honeycomb filters  $F1$ . The outer shape cutting process was performed to manufacture an

assembly 9g (160 mm × 80 mm × 150 mm) having a substantially elliptical cross section, as shown in Fig. 8(a). In the same manner, the assembly of examples 3-2 to 3-4 were manufactured.

5

(Comparative examples 3-1 to 3-4)

The assembly was also manufactured basically in the same way as in example 3-1 in comparative examples 3-1 to 3-4. However, in comparative example 3-1, the dimension D1 was changed to 1.5 mm, and D2 was changed to 1.5 mm. Therefore, ratio  $D1/D2=1$ . After assembling the honeycomb filters F1 in three rows and five columns, the outer shape cutting process was performed to manufacture an assembly 9h (160 mm × 80 mm × 150 mm) having a substantially elliptical cross section, as shown in Fig. 8(b). In comparative example 3-2, the dimension D1 was 0.35 mm, and D2 was 0.4mm. Therefore, ratio  $D1/D2=0.88$ . Five of such honeycomb filters F1 were arranged parallel to D2 and three honeycomb filters F1 were arranged perpendicular to D2 to form an assembly of fifteen honeycomb filters F1. The outer shape cutting process was performed to manufacture an assembly 9i (160 mm × 80 mm × 150 mm) having a substantially elliptical cross section, as shown in Fig. 8(c). The comparative example 3-3 was manufactured in the same manner as in comparative example 3-2, and comparative example 3-4 was manufactured in the same manner as in example 3-1.

With respect to the assembly of examples 3-1 to 3-4, and comparative examples 3-1 to 3-4, the maximum temperature difference  $\Delta T$  and the occurrence of cracks were studied. As a result, as shown in table 9, the maximum temperature difference  $\Delta T$  ( $^{\circ}\text{C}$ ) was  $91^{\circ}\text{C}$  or less in examples 3-1 to 3-4.

Further, no residual soot was present and the occurrence of cracks was not recognized in any of the honeycomb filters F1.

5           However, in comparative example 3-1, comparative example 3-2, and comparative example 3-3, the maximum temperature difference  $\Delta T$  ( $^{\circ}\text{C}$ ) was greater than or equal to approximately  $95^{\circ}\text{C}$ , the value of which is very large.

Further, residual soot was present and the occurrence of  
10 cracks was confirmed in the honeycomb filter F1 at position  $\gamma$ . Further, in comparative example 3-4, the temperature difference was low but cracks occurred.

(Examples 3-5 to 3-8, comparative examples 3-5 to 3-8)

15           In the same manner, similar tests were performed on a silicon carbide - metal silicon filter.

More specifically, in examples 3-5 to 3-8, an assembly  
20 formed by arranging the filters of test examples 6.1 to 6.4 (table 6), as shown in Fig. 8(a), was used. In comparative example 3-5, an assembly formed by arranging the filters of the test reference example 6.3, as shown in Fig. 8(b), was used. In comparative example 3-6 and comparative example 3-  
25 7, assemblies formed by arranging the filters of test examples 6.1 and 6.4 (table 6), respectively, as shown in Fig. 8(c), were used. In comparative example 3-8, an assembly formed by arranging the filters of test comparative example 6.1, as shown in Fig. 8(a) was used.

30           As shown in table 9, the maximum temperature difference of examples 3-5 to 3-8 was  $101^{\circ}\text{C}$  or less. In comparison, in comparative examples 3-5, 3-6, and 3-7, the maximum

temperature difference was 105°C or greater, and cracks occurred in the honeycomb filter located at position  $\gamma$ . In comparative example 3-8, the temperature difference was low, but cracks occurred.

5

(Examples 4-1 to 4-5, comparative examples 4-1 to 4-3)

In examples 4-1 to 4-5, an assembly 9 was manufactured basically in the same manner as in comparative example 1-2 using the filters of the test reference example 1.1 (table 1). In example 4-1, however, the thickness E1 of the sealing material layer 15a was 1.05 mm, the thickness E2 of the sealing material layer 15b was 1 mm, and the ratio  $E1/E2=1.05$  (refer to Fig. 9(a)).

15

Similarly, example 4-2 to example 4-5 and comparative example 4-3 were manufactured in accordance with the description of table 10.

20

In comparative example 4-1, the thickness E1 of the sealing material layer 15a was 1 mm, the thickness E2 of the sealing material layer 15b was 1 mm, and  $E1/E2=1$  (refer to Fig. 9(b)).

25

In comparative example 4-2, the assembly was manufactured basically in the same manner as in comparative example 1-2 using the filters of test reference example 1.1. In example 4-2, however, the thickness E1 of the sealing material layer 15a was 1 mm, the thickness E2 of the sealing material layer 15b was 2 mm, and the ratio  $E1/E2=0.5$  (refer to Fig. 9(c)).

30

With respect to the assemblies of examples 4-1 to 4-5

and comparative examples 4-1 to 4-3, the maximum temperature difference  $T\beta - T\alpha$  and the occurrence of cracks were studied. As a result, as shown in table 10, the maximum temperature difference  $T\beta - T\alpha$  was 75°C or less in examples 4-1 to 4-5, and  
5 no residual soot was present and the occurrence of cracks was not confirmed in any of the honeycomb filters F1.

However, in comparative example 4-1 and comparative example 4-2, the maximum temperature difference  $T\beta - T\alpha$  was  
10 greater than or equal to 80°C, the value of which is very large, and residual soot was present and the occurrence of cracks was confirmed in the honeycomb filter F1 located at position  $\gamma$ . Further, in comparative example 4-3, the temperature difference was reversed and cracks occurred at  
15 position  $\beta$ .

(Examples 4-6 to 4-10, comparative examples 4-4 to 4-6)

In the same manner, similar tests were performed on a  
20 silicon carbide - metal silicon filter.

In example 4-6 to example 4-10, an assembly was manufactured basically in the same manner as in comparative example 1-2 using the filter of the test reference example  
25 2.1. In example 4-6, however, the thickness of the sealing material layer parallel to the long side of the assembly 9 was E1 (1.05 mm), and the thickness of the sealing material layer parallel to the short side was E2 (1 mm), and thus  $E1/E2=1.05$ .

30

Similarly, example 4-6 to example 4-10 and comparative example 4-6 were manufactured in accordance with table 10.



In the assembly of comparative example 4-4, the thickness E1 of the sealing material layer 15a was 1 mm, the thickness E2 of the sealing material layer 15b was 1 mm and thus  $E1/E2=1$  (refer to Fig. 9(b)).

5

In comparative example 4-5, the assembly was manufactured basically in the same manner as in comparative example 1-2 using the filter of test reference example 2.1. In example 4-5, however, the thickness E1 of the sealing material layer 15a was 1 mm, the thickness E2 of the sealing material layer 15b was 2 mm, and the ratio  $E1/E2=0.5$  (refer to Fig. 9(c)).

10

With respect to the assembly of examples 4-6 to 4-10 and comparative examples 4-4 to 4-6, the maximum temperature difference  $T\beta-T\alpha$  and the occurrence of cracks were studied. As a result, as shown in table 10, the maximum temperature difference  $T\beta-T\alpha$  was 80°C or less in the examples, and no residual soot was present and the occurrence of cracks was not confirmed in any of the honeycomb filters F1.

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20

However, in comparative example 4-4 and comparative example 4-5, the maximum temperature difference  $T\beta-T\alpha$  was greater than or equal to 100°C, the value of which is very large, residual soot was present and the occurrence of cracks was confirmed in the honeycomb filter F1 located at position  $\gamma$ . Further, in comparative example 4-6, the temperature difference was reversed and cracks occurred at position  $\beta$ .

25

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(Examples 5-1 to 5-4, comparative examples 5-1 to 5-3)

In examples 5-1 to 5-4, an assembly was manufactured

basically in the same manner as in comparative example 1-2 using the filter of test reference example 1.1 (table 1). In example 5-1, however, the thermal conductivity  $G_1$  of the sealing material layer 15a was  $0.2\text{W/m}\cdot\text{K}$ , the thermal  
5 conductivity  $G_2$  of the sealing material layer 15b was  $0.3\text{W/m}\cdot\text{K}$ , and  $G_1/G_2=0.67$  (refer to Fig. 10(a)).

Similarly, in example 5-2 to example 5-4 and comparative examples 5-1 to 5-3, assemblies were  
10 manufactured by adjusting  $G_1$  in accordance with the description of table 11.

In comparative example 5-1,  $G_1$  and  $G_2$  were the same and thus  $G_1/G_2=1$ .  
15

With respect to the assemblies of examples 5-1 to 5-4 and comparative examples 5-1 to 5-3, the maximum temperature difference  $T_\beta-T_\alpha$  and the occurrence of cracks were studied. As a result, as shown in table 11, the maximum temperature  
20 difference  $T_\beta-T_\alpha$  was  $76^\circ\text{C}$  or less in examples 5-1 to 5-4, and no residual soot was present and the occurrence of cracks was not confirmed in any of the honeycomb filters F1.

However, in comparative example 5-1 and comparative  
25 example 5-2, the maximum temperature difference  $T_\beta-T_\alpha$  was greater than or equal to  $80^\circ\text{C}$ , the value of which is very large, and residual soot was present and the occurrence of cracks were confirmed in the honeycomb filter F1 located at position  $\gamma$ . Further, in comparative example 5-3, the  
30 temperature difference was reversed and cracks occurred at position  $\beta$ .

(Examples 5-5 to 5-8, comparative examples 5-4 to 5-6)

In the same manner, similar tests were performed on a silicon carbide - metal silicon filter.

5 In example 5-5 to example 5-8 and comparative example 5-4 to comparative example 5-6, an assembly was basically manufactured in accordance with the description of table 11 using the filter of test reference example 2.1.

10 In examples 5-5 to 5-8, the temperature difference  $T\beta - T\alpha$  was  $80^{\circ}\text{C}$  or less, and no residual soot was present and the occurrence of cracks was not confirmed in any of the honeycomb filters F1.

15 However, in comparative example 5-4 and comparative example 5-5, the maximum temperature difference  $T\beta - T\alpha$  was greater than or equal to  $80^{\circ}\text{C}$ , the value of which is very large, and residual soot was present and the occurrence of cracks was confirmed in the honeycomb filter F1 located at position  $\gamma$ . Further, in comparative example 5-6, the  
20 temperature difference was reversed and cracks occurred at position  $\beta$ .

The results are shown in table 11.

25 (Example 6-1 to 6-4, comparative example 6-1 to 6-3)

In examples 6-1 to 6-4, an assembly was manufactured basically in the same manner as in comparative example 1-2 using the filter of test reference example 1.1. In example  
30 6-1, however, the thickness H1 of the outer sealing material layer 15c was 1.6mm, thickness H2 of the outer sealing material layer 15d was 1.5 mm, and thus  $H2/H1=0.94$  (refer to Fig. 10(b)). The thickness between the outer sealing

material layers 15c and 15d was adjusted so that the thicknesses of the outer sealing material layers were gradually changed. Therefore, the thicknesses H1 and H2 were either the maximum thickness or the minimum thickness  
5 of the outer sealing material layer.

Similarly, the assembly of example 6-2 to example 6-4, and comparative examples 6-1 to 6-3 were manufactured by adjusting the thickness of H2 in accordance with the  
10 description of table 12.

In comparative example 6-1,  $H2/H1=1$ .

As shown in table 12, in examples 6-1 to 6-4, the  
15 maximum temperature difference  $T\beta-T\alpha$  was 73°C or less and no residual soot was present and the occurrence of cracks was not confirmed in any of the honeycomb filters F1.

However, in comparative example 6-1 and comparative  
20 example 6-2, the maximum temperature difference  $T\beta-T\alpha$  was 80°C or greater, the value of which is very large, and residual soot was present and the occurrence of cracks was confirmed in the honeycomb filter F1 located at position  $\gamma$ . Further, in comparative example 6-3, the temperature  
25 difference was reversed and cracks occurred at position  $\beta$ .

(Examples 6-5 to 6-8, comparative examples 6-4 to 6-6)

In the same manner, similar tests were performed on a  
30 silicon carbide - metal silicon filter.

Example 6-5 to example 6-8 and comparative example 6-4 to comparative example 6-6 were basically manufactured in

accordance with the description of table 12 using the filter of the test reference example 2.1.

As shown in table 12, in examples 6-5 to 6-8, the temperature difference  $T\beta - T\alpha$  was 80°C or less. Further, no residual soot was present and the occurrence of cracks was not confirmed in any of the honeycomb filters F1.

However, in comparative example 6-4 and comparative example 6-5, the maximum temperature difference  $T\beta - T\alpha$  was greater than or equal to 83°C, the value of which is very large. Further, residual soot was present and the occurrence of cracks was confirmed in the honeycomb filter F1 located at position  $\gamma$ . Further, in comparative example 6-6, the temperature difference was reversed and cracks occurred at the position of  $\beta$ .

(Examples 7-1 to 7-3, comparative examples 7-1 to 7-3)

In examples 7-1 to 7-3, an assembly was manufactured basically in the same manner as in comparative example 1-2 using the filter of test reference example 1.1. In example 7-1, however, the thickness I1 of portion 16a of the outer thermal insulation material (mat made of alumina fiber) was 10 mm, the thickness I2 of portion 16b was 11 mm, and  $I2/I1=0.91$  (refer to Fig. 10(c)). The thickness between portion 16a and 16b was adjusted so that the thickness of the thermal insulation material 10 was gradually changed. Therefore, the thicknesses H1 and H2 were either the maximum thickness or the minimum thickness of the thermal insulation material.

In the same manner, example 7-2 to example 7-3 and

comparative example 7-3 were manufactured by adjusting the thickness of I2 in accordance with the description of table 13.

5           In comparative example 7-1, I1 and I2 had the same thickness as in  $H2/H1=1$ .

As shown in table 13, in examples 7-1 to 7-8, the maximum temperature difference  $T\beta-T\alpha$  was 73°C or less.

10          Further, no residual soot was present and the occurrence of cracks was not recognized in any of the honeycomb filters F1.

However, in comparative example 7-1 and comparative  
15          example 7-2, the maximum temperature difference  $T\beta-T\alpha$  was greater than or equal to 80°C, the value of which is very large. Further, the residual soot was present and the occurrence of cracks was confirmed in the honeycomb filter F1 located at position  $\gamma$ . Further, in comparative example 7-  
20          3, the temperature difference was reversed and cracks occurred at position  $\beta$ .

(Examples 7-4 to 7-6, comparative examples 7-4 to 7-6)

25          In the same manner, similar tests were performed on a silicon carbide - metal silicon filter.

Example 7-4 to example 7-6 and comparative example 7-4 to comparative example 7-6 were basically manufactured in  
30          accordance with the description of table 13 using the filter of test reference example 2.1.

The temperature difference  $T\beta-T\alpha$  was 80°C or less in

examples 7-4 to 7-6. Further, no residual soot was present and the occurrence of cracks was not confirmed in any of the honeycomb filters F1.

5           However, in comparative example 7-4 and comparative example 7-5, the maximum temperature difference  $T_{\beta}-T_{\alpha}$  was greater than or equal to 83°C, the value of which is very large. Further, residual soot was present and the occurrence of cracks was confirmed in the honeycomb filter  
10 F1 located at position  $\gamma$ . Further, in comparative example 7-6, the temperature difference was reversed and cracks occurred at position  $\beta$ .

          The present embodiment has the advantages described  
15 below.

(1) The assembly 9 is manufactured by adhering a plurality of ceramic filters F1 so that the long sides of ceramic filters F1 having rectangular cross sections extend  
20 in the direction of the major axis of the assembly 9 and the short sides of the ceramic filters F1 extend in the direction of the minor axis of the assembly 9. Thus, in the major axis direction of the assembly 9, the number of ceramic sealing material layers 15b that may influence  
25 thermal conductivity is reduced. Therefore, the thermal conductivity in the major axis direction is higher than the thermal conductivity in the minor axis direction of the assembly 9 during use, and the filters F1 at the peripheral portion in the major axis direction are more easily heated.  
30 The residual soot is thus not present and cracks do not occur. Further, this may be achieved by changing the ceramic structure without changing the material of the ceramic filter thereby reducing costs.

Further, in such a method, when a hypothetical first straight line intersects the generally elliptical contour at two points in which the distance therebetween is maximum and a hypothetical second straight line orthogonal to the first  
5 straight line intersects the generally elliptical contour at two points in which the distance therebetween is maximum, the number of sealing material layers the first straight line of the assembly traverses is less than or equal to the number of sealing material layers the second straight line  
10 traverses. This reduces thermal conduction obstacles between filters.

(2) The rectangular cells 12 in the columnar honeycomb filters F1 produce a deviation of thermal conduction in the  
15 cross section of the filter. That is, the thermal conductivity in the long side direction of each cell is higher than the thermal conductivity in the short side direction of the cell. The assembly may be formed by arranging the cells so that their long sides are parallel to  
20 the major axis direction of and their short sides are parallel to the minor axis direction of the assembly. This results in the thermal conductivity in the major axis direction being greater than the thermal conductivity in the minor axis direction of the assembly during use. Further,  
25 the filters F1 at the peripheral portion in the major axis direction are more easily heated. Thus, residual soot is eliminated and cracks do not occur. Further, this is easily achieved by changing the ceramic structure without changing the material of the ceramic filter. Thus, costs are  
30 reduced.

(3) The cells 12 in the columnar honeycomb filter F1 are rectangular. By changing the thicknesses of cell walls



that are orthogonal to each other, deviation of the thermal conductivity may be produced along the cross section of the filter. That is, the thermal conductivity in the direction in which the thick cell walls extend is higher than the thermal conductivity in the direction in which the thin cell walls extend. The filter assembly may be formed so that the major axis direction of the assembly is parallel to the direction in which the thick cell walls extend and the minor axis direction of the assembly is parallel to the direction in which the thin cell walls extend. This results in the thermal conductivity in the major axis direction being higher than the thermal conductivity in the minor axis direction of the assembly during use. Further, the filters F1 at the peripheral portion in the major axis direction are more easily heated. Thus, residual soot is eliminated and cracks do not occur. Further, this is easily achieved by changing the ceramic structure without changing the material of the ceramic filter. Thus, costs are reduced.

(4) By making the sealing material layers 15b, which are perpendicular to the major axis direction, relatively thin, the thermal conductivity in the major axis direction becomes higher than the thermal conductivity in the minor axis direction of the assembly 9. Thus, the filters F1 at the peripheral portion in the major axis direction are more easily heated, residual soot is eliminated, and cracks do not occur. Further, this is easily achieved by changing the ceramic structure without changing the material of the ceramic filter. Thus, costs are reduced.

(5) By changing the thermal conductivity G2 of the sealing material layers 15b, which are perpendicular to the major axis direction, to a high value, the thermal

conductivity in the major axis direction becomes higher than in the minor axis direction of the assembly during use. Thus, the filters F1 at the peripheral portion in the major axis direction are more easily heated, residual soot is  
5 eliminated, and cracks do not occur. Further, this is easily achieved by changing the ceramic structure without changing the material of the ceramic filter. Thus, costs are reduced.

10 (6) In the ceramic filter assembly having a generally elliptical cross section, with regards to the outer sealing material layer, which inhibits thermal conduction, the thickness H1 of the sealing material layer located along an extension of the major axis is greater than the thickness H2  
15 of the sealing material layer located along an extension of the minor axis to suppress heat radiation from the peripheral portion in the major axis direction. This produces a high thermal insulation effect at the peripheral portion in the major axis direction. Thus, residual soot is  
20 eliminated, and cracks do not occur. Further, this is easily achieved by changing the ceramic structure without changing the material of the ceramic filter. Thus, costs are reduced.

25 (7) In the ceramic filter assembly 9 having a generally elliptical cross sectional shape, with regards to the thickness of the thermal insulation material 10 that inhibits thermal conduction, the thickness I1 of portion 16a located along an extension of the major axis is greater than  
30 the thickness I2 of portion 16b located along an extension of the minor axis. This suppresses heat radiation from the peripheral portion in the major axis direction. Thus, a high thermal insulation effect is produced at the peripheral

portion in the major axis direction during use of the assembly. Thus, residual soot is eliminated, and cracks do not occur. Further, this is easily achieved by changing the ceramic structure without changing the material of the ceramic filter. Thus, costs are reduced.

(8) According to tests 1 and 2, when the cross sectional shape of a columnar honeycomb filter made of a porous ceramic sintered body is rectangular and the length of the long side is  $B_1$  and the length of the short side is  $B_2$ , if the ratio  $B_1/B_2$  is 3.0 or less, cracking due to thermal shock is less likely to occur. Thus, thermal shock resistance is considered to be about the same as when the cross sectional shape is square, and a filter unit necessary for a uniform temperature rise of the flat shape filter assembly 9 is provided. Since the sealing material and the like may be reduced, costs are also reduced.

(9) According to tests 3 and 4, when the cross sectional shape of a cell (through hole) of a columnar honeycomb filter made of porous ceramic sintered body is rectangular and the length of the long side is  $C_1$  and the length of the short side is  $C_2$ , if the ratio  $C_1/C_2$  is 3.0 or less, cracking due to thermal shock is less likely to occur. Thus, the thermal shock resistance is considered to be about the same as when the cross sectional shape of the cell (through hole) is square, and a filter unit necessary for a uniform temperature rise of the flat shaped filter assembly 9 is provided.

(10) According to tests 5 and 6, when there are two wall thicknesses for a cell of a columnar honeycomb filter made of porous ceramic sintered body and the dimension of

the thick wall is D1 and the dimension of the thin wall is D2, if the ratio D1/D2 is 3.0 or less, cracking due to thermal shock is less likely to occur. Thus, the thermal shock resistance is considered to be about the same as when all of the wall thicknesses are the same, and a filter unit necessary for a uniform temperature rise of the oblong filter assembly 9 is provided.

The embodiment of the present invention may be modified in the following way.

The cross sectional shape of the honeycomb filters F1 may be rectangular, and the inner cells 12 may be rectangular in the same direction.

The cross sectional shape of the honeycomb filters F1 may be rectangular, and the thicker wall 13a of the inner cell walls 13a, 13b may be rectangular in the same direction as the long side.

Each cell of the honeycomb filter may be rectangular and the cell wall of the long side may be thicker than the cell wall of the short side.

The sealing material layer formed on the outer peripheral face of the assembly may be formed using two or more types of coating materials, which are applied to the outer surface, having different thermal conductivity.

The thermal insulation material 10 may be formed on the peripheral surface of the assembly using two or more types of thermal insulation materials having different thermal conductivity.

Table 1

	side length (mm)	wall thickness (mm)	pitch (mm)	cell column number	outer dimension (mm)	outer dimension (mm)	thermal shock test	
							600°C	800°C
	C1, C2	D1, D2			B1	B2		
test reference example 1.1	1.5	0.3	1.8	18	32.7	32.7	1.00	no cracks
test reference example 1.2	1.5	0.3	1.8	19	34.5	32.7	1.06	no cracks
test example 1.1	1.5	0.3	1.8	20	36.3	32.7	1.11	no cracks
test example 1.2	1.5	0.3	1.8	37	66.9	32.7	2.05	no cracks
test example 1.3	1.5	0.3	1.8	54	97.5	32.7	2.98	no cracks
test comparative example 1.1	1.5	0.3	1.8	55	99.3	32.7	3.04	cracks found
test comparative example 1.2	1.5	0.3	1.8	56	101.1	32.7	3.09	cracks found

Table 2

	side length (mm)	wall thickness (mm)	pitch (mm)	cell column number	outer dimension (mm)	outer dimension (mm)	thermal shock test	
							600°C	800°C
	C1, C2	D1, D2			B1	B2		
test reference example 2.1	1.5	0.3	1.8	18	32.7	32.7	1.00	no cracks
test reference example 2.2	1.5	0.3	1.8	19	34.5	32.7	1.06	no cracks
test example 2.1	1.5	0.3	1.8	20	36.3	32.7	1.11	no cracks
test example 2.2	1.5	0.3	1.8	38	68.7	32.7	2.10	no cracks
test example 2.3	1.5	0.3	1.8	54	97.5	32.7	2.98	no cracks
test comparative example 2.1	1.5	0.3	1.8	55	99.3	32.7	3.04	cracks found
test comparative example 2.2	1.5	0.3	1.8	56	101.1	32.7	3.09	cracks found

Table 3

	side length (mm)	wall thickness (mm)	pitch (mm)	cell column number	outer dimension (mm)	side length (mm)	side length (mm)	thermal shock test	
								600°C	800°C
	C1	D1, D2			B1, B2	C1	C2		
test reference example 3.1	1.5	0.3	1.8	18	32.7	1.5	1.5	no cracks	no cracks
test reference example 3.2	1.6	0.3	1.9	17	32.6	1.6	1.5	no cracks	no cracks
test example 3.1	1.7	0.3	2	16	32.3	1.7	1.5	no cracks	no cracks
test example 3.2	2.25	0.3	2.55	13	33.45	2.25	1.5	no cracks	no cracks
test example 3.3	3	0.3	3.3	10	33.3	3	1.5	no cracks	no cracks
test example 3.4	4.4	0.3	4.7	7	33.2	4.4	1.5	no cracks	no cracks
test comparative example 3.1	4.6	0.3	4.9	7	34.6	4.6	1.5	cracks found	cracks found
test comparative example 3.2	4.8	0.3	5.1	6	30.9	4.8	1.5	cracks found	cracks found

Table 4

	side length (mm)	wall thickness (mm)	pitch (mm)	cell column number	outer dimension (mm)	side length (mm)	side length (mm)	C1/C2	thermal shock test	
									600°C	800°C
	C1	D1, D2			B1, B2	C1	C2			
test reference example 4.1	1.5	0.3	1.8	18	32.7	1.5	1.5	1.00	no cracks	no cracks
test reference example 4.2	1.6	0.3	1.9	17	32.6	1.6	1.5	1.07	no cracks	no cracks
test example 4.1	1.7	0.3	2	16	32.3	1.7	1.5	1.13	no cracks	no cracks
test example 4.2	2.25	0.3	2.55	13	33.45	2.25	1.5	1.50	no cracks	no cracks
test example 4.3	3	0.3	3.3	10	33.3	3	1.5	2.00	no cracks	no cracks
test example 4.4	4.4	0.3	4.7	7	33.2	4.4	1.5	2.93	no cracks	no cracks
test comparative example 4.1	4.6	0.3	4.9	7	34.6	4.6	1.5	3.07	no cracks	cracks found
test comparative example 4.2	4.8	0.3	5.1	6	30.9	4.8	1.5	3.20	cracks found	cracks found



Table 5

	side length (mm)	wall thickness (mm)	pitch (mm)	cell column number	outer dimension (mm)	wall thickness (mm)	wall thickness (mm)	D1/D2	thermal shock test	
	C1, C2	D2			B1, B2	D1	D2		600°C	800°C
test reference example 5.1	1.5	0.4	1.9	18	34.6	0.4	0.4	1.00	no cracks	no cracks
test reference example 5.2	1.5	0.37	1.87	18	34.03	0.4	0.37	1.08	no cracks	no cracks
test reference example 5.3	1.5	0.3	1.8	18	32.7	0.3	0.3	1.00	no cracks	no cracks
test example 5.1	1.5	0.35	1.85	18	33.65	0.4	0.35	1.14	no cracks	no cracks
test example 5.2	1.5	0.2	1.7	20	34.2	0.4	0.2	2.00	no cracks	no cracks
test example 5.3	1.5	0.14	1.64	20	32.94	0.4	0.14	2.86	no cracks	no cracks
test example 5.4	1.5	0.15	1.65	20	33.15	0.3	0.15	2.00	no cracks	no cracks
test comparative example 5.1	1.5	0.132	1.632	20	32.772	0.4	0.132	3.03	cracks found	cracks found
test comparative example 5.2	1.5	0.13	1.63	20	32.73	0.4	0.13	3.08	cracks found	cracks found

Table 6

	side length (mm)	wall thickness	pitch (mm)	cell column	outer dimension	wall thickness (mm)	wall thickness (mm)	D1/D2	thermal shock test	
									600°C	800°C
	C1, C2	D2			B1, B2	D1	D2			
test reference example 6.1	1.5	0.4	1.9	18	34.6	0.4	0.4	1.00	no cracks	no cracks
test reference example 6.2	1.5	0.37	1.87	18	34.03	0.4	0.37	1.08	no cracks	no cracks
test reference example 6.3	1.5	0.3	1.8	18	32.7	0.3	0.3	1.00	no cracks	no cracks
test example 6.1	1.5	0.35	1.85	18	33.65	0.4	0.35	1.14	no cracks	no cracks
test example 6.2	1.5	0.2	1.7	20	34.2	0.4	0.2	2.00	no cracks	no cracks
test example 6.3	1.5	0.14	1.64	20	32.94	0.4	0.14	2.86	no cracks	no cracks
test example 6.4	1.5	0.15	1.65	20	33.15	0.3	0.15	2.00	no cracks	no cracks
test comparative example 6.1	1.5	0.132	1.632	20	32.772	0.4	0.132	3.03	no cracks found	cracks found
test comparative example 6.2	1.5	0.13	1.63	20	32.73	0.4	0.13	3.08	cracks found	cracks found

Table 7

	shape	type	assembly 9			filter F1			cell 12			cell wall 13			sealing material layer 15			peripheral portion	insulation	Temp. difference $\Delta T$	temperature			cracks
			A1	A2	mm	B1	B2	quantit v	C1	C2	C1/C2	D1	D2	D1/D2	E1	E2	E1/E2	mm	mm	$^{\circ}C$	$\alpha$	$\beta$	$\gamma$	
example 1-1	Fig. 6(a)	test example 1.2	160	80	mm	66	33	9	1.50	1.50	1.00	0.3	0.3	1.00	1	1	1	1.5	10	50	450	430	400	none
comparative example 1-1	Fig. 6(b)	test reference example 1.1	80	80	mm	33	33	9	1.50	1.50	1.00	0.3	0.3	1.00	1	1	1	1.5	10	50	450	430	400	none
comparative example 1-2	Fig. 6(c)	test reference example 1.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	1	1	1	1.5	10	100	450	430	350	found
example 1-2	Fig. 6(a)	test example 2.2	160	80	mm	66	33	9	1.50	1.50	1.00	0.3	0.3	1.00	1	1	1	1.5	10	60	450	424	390	none
comparative example 1-3	Fig. 6(b)	test example 2.1	80	80	mm	33	33	9	1.50	1.50	1.00	0.3	0.3	1.00	1	1	1	1.5	10	60	450	425	390	none
comparative example 1-4	Fig. 6(c)	test example 2.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	1	1	1	1.5	10	110	450	423	340	found

Table 8

	shape	type	assembly 9			filter F1			cell 12			cell wall 13			sealing material layer 15			peripheral portion	insulation	temperature difference	temperature			cracks
			A1	A2	B1	B2	quantit y		C1	C2	C1/C2	D1	D2	D1/D2	E1	E2	E1/E2			$\Delta T$	$\alpha$	$\beta$	$\gamma$	
example 2-1	Fig. 7(a)	test example 3.1	160	80	33	33	15		1.70	1.50	1.13	0.3	0.3	1.00	1	1	1	1.5	10	93	450	430	357	none
example 2-2	Fig. 7(a)	test example 3.2	160	80	33	33	15		2.25	1.50	1.50	0.3	0.3	1.00	1	1	1	1.5	10	80	450	430	370	none
example 2-3	Fig. 7(a)	test example 3.3	160	80	33	33	15		3.00	1.50	2.00	0.3	0.3	1.00	1	1	1	1.5	10	76	450	430	374	none
example 2-4	Fig. 7(a)	test example 3.4	160	80	33	33	15		4.40	1.50	2.93	0.3	0.3	1.00	1	1	1	1.5	10	70	450	430	380	none
comparative example 2-1	Fig. 7(b)	test reference example 3.1	160	80	33	33	15		1.50	1.50	1.00	0.3	0.3	1.00	1	1	1	1.5	10	100	450	430	350	found
comparative example 2-2	Fig. 7(c)	test reference example 3.1	160	80	33	33	15		1.50	1.70	0.88	0.3	0.3	1.00	1	1	1	1.5	10	100	450	434	350	found
comparative example 2-3	Fig. 7(c)	test reference example 3.2	160	80	33	33	15		1.50	2.25	0.67	0.3	0.3	1.00	1	1	1	1.5	10	100	450	440	350	found
comparative example 2-4	Fig. 7(a)	test reference example 3.1	160	80	33	33	15		4.60	1.50	3.07	0.3	0.3	1.00	1	1	1	1.5	10	65	450	430	385	found
example 2-5	Fig. 7(c)	test example 4.1	160	80	33	33	15		1.70	1.50	1.13	0.3	0.3	1.00	1	1	1	1.5	10	103	450	423	347	none
example 2-6	Fig. 7(a)	test example 4.2	160	80	33	33	15		2.25	1.50	1.50	0.3	0.3	1.00	1	1	1	1.5	10	90	450	423	360	none
example 2-7	Fig. 7(a)	test example 4.3	160	80	33	33	15		3.00	1.50	2.00	0.3	0.3	1.00	1	1	1	1.5	10	86	450	423	364	none
example 2-8	Fig. 7(a)	test example 4.4	160	80	33	33	15		4.40	1.50	2.93	0.3	0.3	1.00	1	1	1	1.5	10	80	450	423	370	none
comparative example 2-5	Fig. 7(b)	test reference example 4.1	160	80	33	33	15		1.50	1.50	1.00	0.3	0.3	1.00	1	1	1	1.5	10	110	450	423	340	found
comparative example 2-6	Fig. 7(c)	test reference example 4.1	160	80	33	33	15		1.50	1.70	0.88	0.3	0.3	1.00	1	1	1	1.5	10	120	450	434	340	found
comparative example 2-7	Fig. 7(c)	test reference example 4.2	160	80	33	33	15		1.50	2.25	0.67	0.3	0.3	1.00	1	1	1	1.5	10	110	450	440	340	found
comparative example 2-8	Fig. 7(a)	test reference example 4.1	160	80	33	33	15		4.60	1.50	3.07	0.3	0.3	1.00	1	1	1	1.5	10	75	450	430	375	found

Table 9

	shape	type	assembly 9		filter F1		cell 12			cell wall 13			sealing material layer 15			peripheral portion	insulation	Temp. difference	temperature			cracks	
			A1 mm	A2 mm	B1 mm	B2 mm	quant y number	C1 mm	C2 mm	C1/C2	D1 mm	D2 mm	D1/D2	E1 mm	E2 mm	E1/E2	mm	mm	ΔT °C	α °C	β °C		γ °C
example 3-1	Fig. 8(a)	test example 5.1	160	80	33	33	15	1.50	1.50	1.00	0.4	0.35	1.14	1	1	1	1.5	10	91	450	423	359	none
example 3-2	Fig. 8(a)	test example 5.2	160	80	33	33	15	1.50	1.50	1.00	0.4	0.2	2.00	1	1	1	1.5	10	79	450	428	371	none
example 3-3	Fig. 8(a)	test example 5.3	160	80	33	33	15	1.50	1.50	1.00	0.4	0.14	2.86	1	1	1	1.5	10	73	450	424	377	none
example 3-4	Fig. 8(a)	test example 5.4	160	80	33	33	15	1.50	1.50	1.00	0.3	0.15	2.00	1	1	1	1.5	10	85	450	425	365	none
comparative example 3-1	Fig. 8(b)	test reference example 5.3	160	80	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	1	1	1	1.5	10	100	450	430	350	found
comparative example 3-2	Fig. 8(c)	test example 5.1	160	80	33	33	15	1.50	1.50	1.00	0.35	0.4	0.88	1	1	1	1.5	10	95	450	435	355	found
comparative example 3-3	Fig. 8(c)	test example 5.4	160	80	33	33	15	1.50	1.50	1.00	0.15	0.3	0.50	1	1	1	1.5	10	110	450	430	340	found
comparative example 3-4	Fig. 8(a)	test comparative example 5.1	160	80	33	33	15	1.50	1.50	1.00	0.4	0.132	3.03	1	1	1	1.5	10	68	450	430	382	found
example 3-5	Fig. 8(a)	test example 6.1	160	80	33	33	15	1.50	1.50	1.00	0.4	0.35	1.14	1	1	1	1.5	10	101	450	416	349	none
example 3-6	Fig. 8(a)	test example 6.2	160	80	33	33	15	1.50	1.50	1.00	0.4	0.2	2.00	1	1	1	1.5	10	90	450	420	360	none
example 3-7	Fig. 8(a)	test example 6.3	160	80	33	33	15	1.50	1.50	1.00	0.4	0.14	2.86	1	1	1	1.5	10	82	450	415	368	none
example 3-8	Fig. 8(a)	test example 6.4	160	80	33	33	15	1.50	1.50	1.00	0.3	0.15	2.00	1	1	1	1.5	10	95	450	413	355	none
comparative example 3-5	Fig. 8(b)	test reference example 6.3	160	80	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	1	1	1	1.5	10	110	450	423	340	found
comparative example 3-6	Fig. 8(c)	test example 6.1	160	80	33	33	15	1.50	1.50	1.00	0.35	0.4	0.88	1	1	1	1.5	10	105	450	428	345	found
comparative example 3-7	Fig. 8(c)	test example 6.4	160	80	33	33	15	1.50	1.50	1.00	0.15	0.3	0.50	1	1	1	1.5	10	120	450	423	330	found
comparative example 3-8	Fig. 8(a)	test comparative example 6.1	160	80	33	33	15	1.50	1.50	1.00	0.4	0.132	3.03	1	1	1	1.5	10	75	450	430	375	found

Table 10

	Shape	type	assembly 9			filter F1			cell 12			cell wall 13			sealing material layer			peripheral portion	insulation	Temp. difference	temperature			cracks
			A1	A2	mm	B1	B2	quantit v	C1	C2	C1/C2	D1	D2	D1/D2	E1	E2	E1/E2			$\beta - \gamma$	$\alpha$	$\beta$	$\gamma$	
example 4-1	Fig. 9(a)	test reference example 1.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	1.05	1	1.05	1.5	10	75	450	425	350	none
example 4-2	Fig. 9(a)	test reference example 1.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	2	1	2	1.5	10	75	450	425	350	none
example 4-3	Fig. 9(a)	test reference example 1.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	3	1	3	1.5	10	65	450	415	350	none
example 4-4	Fig. 9(a)	test reference example 1.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	4	1	4	1.5	10	20	450	370	350	none
example 4-5	Fig. 9(a)	test reference example 1.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	5	1	5	1.5	10	0	450	350	350	none
comparative example 4-1	Fig. 9(b)	test reference example 1.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	1	1	1	1.5	10	80	450	430	350	found
comparative example 4-2	Fig. 9(c)	test reference example 1.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	1	2	0.5	1.5	10	130	450	440	310	found
comparative example 4-3	Fig. 9(a)	test reference example 1.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	6	1	6	1.5	10	-20	450	330	350	found
example 4-6	Fig. 9(a)	test reference example 2.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	1.05	1	1.05	1.5	10	75	450	415	340	none
example 4-7	Fig. 9(a)	test reference example 2.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	2	1	2	1.5	10	75	450	415	340	none
example 4-8	Fig. 9(a)	test reference example 2.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	3	1	3	1.5	10	71	450	411	340	none
example 4-9	Fig. 9(a)	test reference example 2.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	4	1	4	1.5	10	25	450	365	340	none
example 4-10	Fig. 9(a)	test reference example 2.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	5	1	5	1.5	10	2	450	342	340	none
comparative example 4-4	Fig. 9(b)	test reference example 2.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	1	1	1	1.5	10	83	450	423	340	found
comparative example 4-5	Fig. 9(c)	test reference example 2.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	1	2	0.5	1.5	10	132	450	432	300	found
comparative example 4-6	Fig. 9(a)	test reference example 2.1	160	80	mm	33	33	15	1.50	1.50	1.00	0.3	0.3	1.00	6	1	6	1.5	10	-10	450	330	340	found

Table 11

	shape	type	assembly 9			filter F1			cerami c fibers	SiC	silica sol	CMC	water	sealing material layer 15			thermal conductivity			peripheral portion	insulati on	Temp. difference	temperature			cracks					
			long axis A1	short axis A2	long side B1	short side B2	short side B2	quant v						average diameter 0.3 μm	wt%	wt%	wt%	E1	E2				E1/E2	long axis G1	short axis G2		W/m <sup>2</sup> K	W/m <sup>2</sup> K	α	β	γ
example 5-1	Fig. 10(a)	test reference example 1.1	160	80	33	33	15	31.10	15.00	14.40	0.50	39.00	1	1	1	0.2	0.3	0.87	1.5	10	76	450	426	350	none						
example 5-2	Fig. 10(a)	test reference example 1.1	160	80	33	33	15	34.00	7.50	19.00	0.50	39.00	1	1	1	0.15	0.3	0.50	1.5	10	75	450	425	350	none						
example 5-3	Fig. 10(a)	test reference example 1.1	160	80	33	33	15	30.30	3.00	27.20	0.50	39.00	1	1	1	0.1	0.3	0.33	1.5	10	65	450	415	350	none						
example 5-4	Fig. 10(a)	test reference example 1.1	160	80	33	33	15	31.30	0.50	28.70	0.50	39.00	1	1	1	0.06	0.3	0.20	1.5	10	0	450	350	350	none						
comparative example 5-1	Fig. 10(b)	test reference example 1.1	160	80	33	33	15	23.30	30.20	7.00	0.50	39.00	1	1	1	0.3	0.3	1.00	1.5	10	80	450	430	350	found						
comparative example 5-2	Fig. 10(c)	test reference example 1.1	160	80	33	33	15	13.50	40.00	7.00	0.50	39.00	1	1	1	0.6	0.3	2.00	1.5	10	90	450	440	350	found						
comparative example 5-3	Fig. 10(a)	test reference example 1.1	160	80	33	33	15	31.30	0.20	29.00	0.50	39.00	1	1	1	0.05	0.3	0.17	1.5	10	-20	450	330	350	found						
example 5-5	Fig. 10(a)	test reference example 2.1	160	80	33	33	15	31.10	15.00	14.40	0.50	39.00	1	1	1	0.2	0.3	0.87	1.5	10	76	450	416	340	none						
example 5-6	Fig. 10(a)	test reference example 2.1	160	80	33	33	15	34.00	7.50	19.00	0.50	39.00	1	1	1	0.15	0.3	0.50	1.5	10	75	450	415	340	none						
example 5-7	Fig. 10(a)	test reference example 2.1	160	80	33	33	15	30.30	3.00	27.20	0.50	39.00	1	1	1	0.1	0.3	0.33	1.5	10	71	450	411	340	none						
example 5-8	Fig. 10(a)	test reference example 2.2	160	80	33	33	15	31.30	0.50	28.70	0.50	39.00	1	1	1	0.06	0.3	0.20	1.5	10	2	450	342	340	none						
comparative example 5-4	Fig. 10(b)	test reference example 2.3	160	80	33	33	15	23.30	30.20	7.00	0.50	39.00	1	1	1	0.3	0.3	1.00	1.5	10	83	450	423	340	found						
comparative example 5-5	Fig. 10(c)	test reference example 2.4	160	80	33	33	15	13.50	40.00	7.00	0.50	39.00	1	1	1	0.6	0.3	2.00	1.5	10	92	450	432	340	found						
comparative example 5-6	Fig. 10(a)	test reference example 2.1	160	80	33	33	15	31.30	0.20	29.00	0.50	39.00	1	1	1	0.05	0.3	0.17	1.5	10	-10	450	330	340	found						

Table 12

	shape	type	assembly 9			filter F1			cerami c fibers	SiC	silica sol	CMC	water	total	sealing material layer 15						outer sealing material				insulation	Temp. difference	temperature		cracks				
			long axis	short axis	mm	long axis	short axis	mm							B1	B2	quantit y	average diameter	wt%	mm	E1	E2	E1/E2	H2			H1	H2/H1		$\beta - \gamma$	$\alpha$	$\beta$	$\gamma$
example 6-1	Fig. 10(a)	test reference example 1.1	160	80	33	33	33	15	23.30	30.20	7.00	0.50	39.00	100.00	1	1	1	1.5	1.6	0.94	10	73	450	423	350	none							
example 6-2	Fig. 10(a)	test reference example 1.1	160	80	33	33	33	15	23.30	30.20	7.00	0.50	39.00	100.00	1	1	1	1.5	10.0	0.15	10	70	450	420	350	none							
example 6-3	Fig. 10(a)	test reference example 1.1	160	80	33	33	33	15	23.30	30.20	7.00	0.50	39.00	100.00	1	1	1	1.5	20.0	0.08	10	60	450	410	350	none							
example 6-4	Fig. 10(a)	test reference example 1.1	160	80	33	33	33	15	23.30	30.20	7.00	0.50	39.00	100.00	1	1	1	1.5	25.0	0.06	10	0	450	350	350	none							
comparative example 6-1	Fig. 10(b)	test reference example 1.1	160	80	33	33	33	15	23.30	30.20	7.00	0.50	39.00	100.00	1	1	1	1.5	1.5	1.00	10	80	450	430	350	found							
comparative example 6-2	Fig. 10(c)	test reference example 1.1	160	80	33	33	33	15	23.30	30.20	7.00	0.50	39.00	100.00	1	1	1	1.5	1.0	1.50	10	90	450	440	350	found							
comparative example 6-3	Fig. 10(a)	test reference example 1.1	160	80	33	33	33	15	23.30	30.20	7.00	0.50	39.00	100.00	1	1	1	1.5	30.0	0.05	10	-30	450	320	350	found							
example 6-5	Fig. 10(a)	test reference example 2.1	160	80	33	33	33	15	23.30	30.20	7.00	0.50	39.00	100.00	1	1	1	1.5	1.6	0.94	10	80	450	420	340	none							
example 6-6	Fig. 10(a)	test reference example 2.1	160	80	33	33	33	15	23.30	30.20	7.00	0.50	39.00	100.00	1	1	1	1.5	10.0	0.15	10	78	450	418	340	none							
example 6-7	Fig. 10(a)	test reference example 2.1	160	80	33	33	33	15	23.30	30.20	7.00	0.50	39.00	100.00	1	1	1	1.5	20.0	0.08	10	68	450	408	340	none							
example 6-8	Fig. 10(a)	test reference example 2.1	160	80	33	33	33	15	23.30	30.20	7.00	0.50	39.00	100.00	1	1	1	1.5	25.0	0.06	10	2	450	342	340	none							
comparative example 6-4	Fig. 10(b)	test reference example 2.1	160	80	33	33	33	15	23.30	30.20	7.00	0.50	39.00	100.00	1	1	1	1.5	1.5	1.00	10	83	450	423	340	found							
comparative example 6-5	Fig. 10(c)	test reference example 2.1	160	80	33	33	33	15	23.30	30.20	7.00	0.50	39.00	100.00	1	1	1	1.5	1.0	1.50	10	98	450	438	340	found							
comparative example 6-6	Fig. 10(a)	test reference example 2.1	160	80	33	33	33	15	23.30	30.20	7.00	0.50	39.00	100.00	1	1	1	1.5	30.0	0.05	10	-10	450	330	340	found							



Table 13

	shape	type	assembly 9		filter F1				sealing material layer 15				outer sealing material				outer insulation material				Temp. difference	temperature		cracks
			long axis	short axis	long axis	short axis	long axis	short axis	long axis	short axis	long axis	short axis	long axis	short axis	long axis	short axis	long axis	short axis						
																			A1	A2		B1	B2	
			mm	mm	mm	mm	mm	number	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm						
example 7-1	Fig. 10(a)	test reference example 1.1	160	80	33	33	33	15	1	1	1	1.5	1.5	1.00	10	11	0.91	73	450	423	350	none		
example 7-2	Fig. 10(a)	test reference example 1.1	160	80	33	33	33	15	1	1	1	1.5	1.5	1.00	10	20	0.50	70	450	420	350	none		
example 7-3	Fig. 10(a)	test reference example 1.1	160	80	33	33	33	15	1	1	1	1.5	1.5	1.00	10	30	0.33	0	450	350	350	none		
comparative example 7-1	Fig. 10(b)	test reference example 1.1	160	80	33	33	33	15	1	1	1	1.5	1.5	1.00	10	10	1.00	80	450	430	350	found		
comparative example 7-2	Fig. 10(c)	test reference example 1.1	160	80	33	33	33	15	1	1	1	1.5	1.5	1.00	10	35	0.29	90	450	440	350	found		
comparative example 7-3	Fig. 10(a)	test reference example 1.1	160	80	33	33	33	15	1	1	1	1.5	1.5	1.00	10	9	1.11	-30	450	320	350	found		
example 7-4	Fig. 10(a)	test reference example 2.1	160	80	33	33	33	15	1	1	1	1.5	1.5	1.0	10	11	0.91	80	450	420	340	none		
example 7-5	Fig. 10(a)	test reference example 2.1	160	80	33	33	33	15	1	1	1	1.5	1.5	1	10	20	0.50	78	450	418	340	none		
example 7-6	Fig. 10(a)	test reference example 2.1	160	80	33	33	33	15	1	1	1	1.5	1.5	1	10	30	0.33	2	450	342	340	none		
comparative example 7-4	Fig. 10(b)	test reference example 2.1	160	80	33	33	33	15	1	1	1	1.5	1.5	1	10	10	1.00	83	450	423	340	found		
comparative example 7-5	Fig. 10(c)	test reference example 2.1	160	80	33	33	33	15	1	1	1	1.5	1.5	1	10	35	0.29	98	450	438	340	found		
comparative example 7-6	Fig. 10(a)	test reference example 2.1	160	80	33	33	33	15	1	1	1	1.5	1.5	1	10	9	1.11	-10	450	330	340	found		